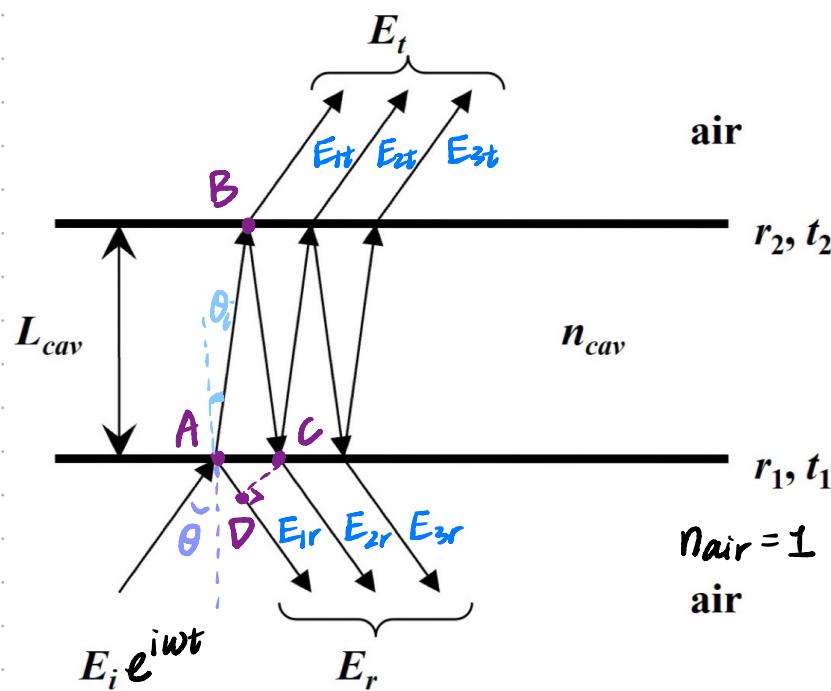


# PHYS-434 Physics of photonic semiconductor devices

## Series 6 - Basic notions on the physics of semiconductor microcavities

1)



We wish to determine the phase shift  $\delta$  associated with the optical path difference between the first reflected beam and the second one:

$$\Delta = n_{\text{cav}}(\overline{AB} + \overline{BC}) - n_{\text{air}} \overline{AD} \quad \overline{AB} = \overline{BC} = \frac{L_{\text{cav}}}{\cos \theta_i}, \quad \overline{AD} = \overline{AC} \sin \theta, \\ \text{Snell law: } \sin \theta = n_{\text{cav}} \sin \theta_i, \quad 2L_{\text{cav}} \tan \theta_i$$

$$= 2n_{\text{cav}}L_{\text{cav}} \frac{1}{\cos \theta_i} - 2n_{\text{cav}}L_{\text{cav}} \frac{\sin^2 \theta_i}{\cos \theta_i} = 2n_{\text{cav}}L_{\text{cav}} \cos \theta_i$$

$$\Rightarrow \delta = \frac{2\pi}{\lambda} \Delta \quad (\text{when neglecting dephasing occurring at the reflection})$$

$$\Rightarrow \delta = \frac{2\pi}{\lambda} (2n_{\text{cav}}L_{\text{cav}} \cos \theta_i)$$

2) The transmitted field is related to the incoming one through:

$$E_{1t} = E_i e^{i\omega t} \cdot t_1 \cdot e^{i\delta_0} \cdot t_2 \quad (\delta_0 = \frac{2\pi}{\lambda} n_{\text{cav}} \overline{AB})$$

$$\begin{aligned}
 E_{2t} &= E_i e^{i\omega t} \cdot t_1 \cdot e^{i80^\circ} \cdot (r_2 \cdot r_1 \cdot e^{i8^\circ}) \cdot t_2 \\
 E_{3t} &= E_i e^{i\omega t} \cdot t_1 \cdot e^{i80^\circ} \cdot (r_2 \cdot r_1 \cdot e^{i8^\circ})^2 \cdot t_2 \\
 &\vdots \\
 E_{Nt} &= E_i e^{i\omega t} \cdot t_1 \cdot e^{i80^\circ} \cdot (r_2 \cdot r_1 \cdot e^{i8^\circ})^{N-1} \cdot t_2
 \end{aligned}
 \quad \left. \begin{aligned}
 E_t &= E_{1t} + E_{2t} + E_{3t} \\
 &\quad + \dots + E_{Nt}
 \end{aligned} \right\}$$

$$\Rightarrow E_t = E_{1t} [1 + r_1 r_2 e^{i8^\circ} + (r_1 r_2 e^{i8^\circ})^2 + \dots + (r_1 r_2 e^{i8^\circ})^{N-1}]$$

(physically  $|r_1 r_2 e^{i8^\circ}| < 1$ , provided  $N \rightarrow \infty$ )

$$E_t = E_{1t} \left[ \frac{1}{1 - r_1 r_2 e^{i8^\circ}} \right] \quad E_{1t} = E_i e^{i(\omega t + \delta_0)} \cdot t_1 t_2$$

geometric series:

$$\sum_{k=0}^{\infty} ar^k \xrightarrow{|r| < 1} \frac{a}{1-r}$$

$$\Rightarrow E_t = E_i e^{i(\omega t + \delta_0)} \left[ \frac{t_1 t_2}{1 - r_1 r_2 e^{i8^\circ}} \right]$$

$$3) T = \left| \frac{E_t}{E_i} \right|^2 = \underbrace{\frac{(t_1 t_2)^2}{|1 - r_1 r_2 \cos \delta - i r_1 r_2 \sin \delta|^2}}$$

$$\begin{aligned}
 (1 - r_1 r_2 \cos \delta)^2 + (r_1 r_2 \sin \delta)^2 &= 1 - 2r_1 r_2 \cos \delta + (r_1 r_2)^2 \\
 &= (1 - r_1 r_2)^2 + 2r_1 r_2 \frac{(1 - \cos \delta)}{2 \sin^2 \frac{\delta}{2}}
 \end{aligned}$$

$$\Rightarrow T = \frac{(t_1 t_2)^2}{(1 - r_1 r_2)^2 + 4r_1 r_2 \sin^2 \left( \frac{\delta}{2} \right)} \quad \text{or} \quad \frac{(t_1 t_2)^2}{1 + (r_1 r_2)^2 - 2r_1 r_2 \cos \delta}$$

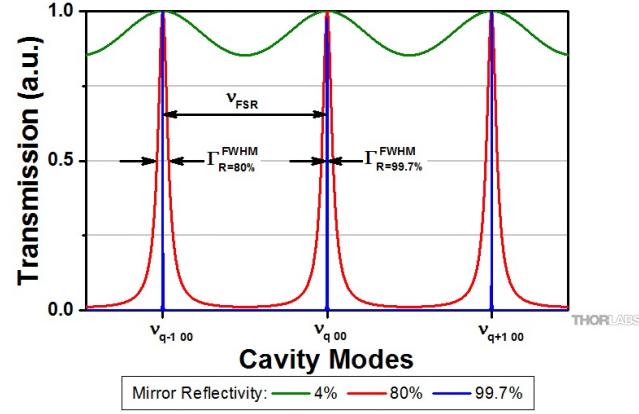
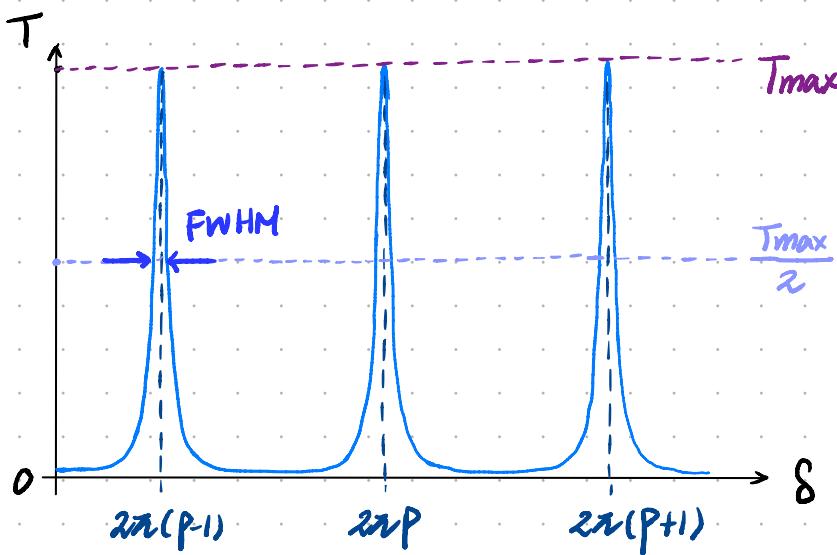
In absence of any optical losses:  $R + T = 1$

$$\begin{aligned}
 4) \text{ Condition of cavity modes: } \delta &= 2\pi p, \quad p = \text{integer} & \text{cavity mode wavelength} \\
 & \quad \uparrow \text{(associated with } E\text{)} \\
 \Rightarrow \frac{2\pi}{\lambda} (2n_{\text{cav}} L_{\text{cav}} \cos \theta_i) &= 2\pi p \Rightarrow 2n_{\text{cav}} L_{\text{cav}} \cos \theta_i = p\lambda
 \end{aligned}$$

⊕ phase at the reflection (depends on energy  $E$ ):  $\phi(E)$

$$\Rightarrow 2n_{\text{car}} L_{\text{car}} \cos \theta_i = (P - \frac{\phi(E)}{2\pi}) \lambda$$

5)



The linewidth (FWHM) of the modes  $\gamma_c$  is obtained by determining  $\delta'$ :

$$T(\delta') = \frac{T_{\max}}{2} \quad \text{with} \quad \delta' = \delta + \varepsilon, \quad \delta = 2\pi P \quad (P = \text{integer}), \quad \varepsilon \ll \delta$$

\* here, everything is calculated with  $T_{\min} \approx 0$ , as shown in the fig. on left, which is generally the case for Fabry Perot cavities in reality ( $R \approx 1$ )

$$T_{\max} = T(\delta) = \frac{(t_1 t_2)^2}{(1 - r_1 r_2)^2}$$

$$\Rightarrow \frac{(t_1 t_2)^2}{2(1 - r_1 r_2)^2} = \frac{(t_1 t_2)^2}{1 + (r_1 r_2)^2 - 2r_1 r_2 \cos \delta'}$$

$$\Rightarrow 1 + 2(r_1 r_2)^2 - 4r_1 r_2 = 1 + (r_1 r_2)^2 - 2r_1 r_2 \cos \delta' \quad \cos \delta' = \cos(2\pi P + \varepsilon)$$

$$\Rightarrow \cos \varepsilon = - \frac{(1 - r_1 r_2)^2 - 2r_1 r_2}{2r_1 r_2} = 1 - \frac{(1 - r_1 r_2)^2}{2r_1 r_2} = \cos \varepsilon$$

$$\varepsilon \ll \delta \quad \Rightarrow \quad 1 - \frac{\varepsilon^2}{\delta^2} = 1 - \frac{(1 - r_1 r_2)^2}{2r_1 r_2} \quad \Rightarrow \quad \varepsilon = \frac{1 - r_1 r_2}{\sqrt{2r_1 r_2}}$$

Based on 4)  $\delta = \frac{2\pi}{\lambda_{\text{cav}}} (2\pi n_{\text{cav}} L_{\text{cav}} \cos\theta_i) = 2\pi P, \quad \cos\theta_i = 1$

( $L_{\text{cav}}$  is large enough that  $\phi(E)$  is neglected) (normal incidence)

$$\Rightarrow |\Delta S| = \frac{4\pi n_{\text{cav}} L_{\text{cav}}}{\lambda_{\text{cav}}^2} \Delta \lambda_{\text{cav}} = \frac{4\pi n_{\text{cav}} L_{\text{cav}}}{\lambda_{\text{cav}}} \cdot \frac{\Delta \lambda_{\text{cav}}}{\lambda_{\text{cav}}} = \frac{2\pi P}{Q}$$

where  $Q = \frac{\lambda_{\text{cav}}}{\Delta \lambda_{\text{cav}}}$  is the quality factor of the Fabry-Perot cavity,  
also known as the resolving power.

At the limit of resolution, we fulfill the equality:  $2\varepsilon = |\Delta S|$

$$\begin{aligned} \text{By definition, } \gamma_c &= \Delta \omega = \Delta \left( \frac{2\pi c}{\lambda} \right) = 2\pi c \frac{\Delta \lambda_{\text{cav}}}{\lambda_{\text{cav}}^2} \\ &= 2\pi c \frac{|\Delta S|}{4\pi n_{\text{cav}} L_{\text{cav}}} = \frac{c \cdot \varepsilon}{n_{\text{cav}} L_{\text{cav}}} \\ \Rightarrow \gamma_c &= \frac{c(1 - r_1 r_2)}{n_{\text{cav}} L_{\text{cav}} \sqrt{r_1 r_2}} \end{aligned}$$

6) Adjacent modes being separated by  $2\pi \Rightarrow F = \frac{2\pi}{2\varepsilon}$

$$\Rightarrow F = \frac{\pi \sqrt{r_1 r_2}}{1 - r_1 r_2}$$

7)  $\vec{k} = \vec{k}_{\parallel} + \vec{k}_z$  and the cavity photon energy is such that:

$$\vec{k}_{\parallel}^2 + \vec{k}_z^2 = \left( \frac{2\pi n_{\text{cav}}}{\lambda} \right)^2$$

under normal incidence:  $\theta = \theta_i = 0$ , which implies that:

$$k_z = \frac{p\pi}{L_{\text{cav}}}$$

and the dispersion of optical modes is then given by:

$$E_c(\vec{k}_{\parallel}) = \frac{\hbar c p\pi}{n_{\text{cav}} L_{\text{cav}}} \left( 1 + \left( \frac{L_{\text{cav}} k_{\parallel}}{p\pi} \right)^2 \right)^{1/2}$$

8) For small  $\vec{k}_{\parallel}$  values:  $E_c(\vec{k}_{\parallel}) \approx \frac{\hbar c P \lambda}{n_{\text{cav}} L_{\text{cav}}} \left( 1 + \frac{L_{\text{cav}}^2 k_{\parallel}^2}{2 P^2 \lambda^2} \right)$

Thus,  $E_c(\vec{k}_{\parallel}) = \frac{\hbar c P \lambda}{n_{\text{cav}} L_{\text{cav}}} + \frac{\hbar c P \lambda L_{\text{cav}}^2 k_{\parallel}^2}{n_{\text{cav}} L_{\text{cav}} 2 P^2 \lambda^2}$

$\Rightarrow E_c(\vec{k}_{\parallel}) = E_c(0) + \frac{\hbar c L_{\text{cav}}}{2 n_{\text{cav}} P \lambda} \vec{k}_{\parallel}^2$  with  $E_c(0) = \frac{\hbar c P \lambda}{n_{\text{cav}} L_{\text{cav}}}$

and finally:  $E_c(\vec{k}_{\parallel}) = E_c(0) + \frac{\hbar^2 \vec{k}_{\parallel}^2}{2 M_{\text{ph}}}$  with  $M_{\text{ph}} = \frac{\hbar P \lambda n_{\text{cav}}}{c L_{\text{cav}}}$

9) If one considers the penetration length  $L_{\text{DBR}}$  and  $\lambda_{\text{DBR}} \approx \lambda_{\text{cav}} \approx \lambda$ :

$$\begin{aligned} L_{\text{cav}} + 2 L_{\text{DBR}} &\approx \frac{P \lambda}{2 n_{\text{cav}}} + 2 \cdot \frac{\lambda}{2} \frac{n_2}{2 \tilde{n} \Delta n} \\ &\approx \frac{P \lambda}{2 n_{\text{cav}}} + \frac{\lambda}{2 n_{\text{cav}}} \underbrace{\frac{n_{\text{cav}} n_2}{\Delta n \tilde{n}}}_{\sim} \sim \frac{n_{\text{cav}}}{\Delta n} \end{aligned}$$

$$\Rightarrow 2 n_{\text{cav}} (L_{\text{cav}} + 2 L_{\text{DBR}}) \approx \underbrace{\left( P + \frac{n_{\text{cav}}}{\Delta n} \right) \lambda}_{\gamma_{\text{eff}} \dots \text{effective order of the cavity}}$$

$$\Rightarrow \gamma_{\text{c}} = \frac{c}{n_{\text{cav}} (L_{\text{cav}} + 2 L_{\text{DBR}})} \frac{1 - r_1 r_2}{\sqrt{r_1 r_2}}$$

10) a) SiO<sub>2</sub>/Si<sub>3</sub>N<sub>4</sub>

The SiO<sub>2</sub>/Si<sub>3</sub>N<sub>4</sub> couple is made of **amorphous** materials characterized by a **wide bandgap** (insulating materials). They are therefore well adapted to cover a wide spectral range (from the IR down to the UV ( $\lambda \approx 300$  nm)).

In addition, costs associated with their deposition are low compared with crystalline semiconductor epitaxy techniques (use of low temperature ( $T < 300^\circ\text{C}$ ))

plasma enhanced chemical vapor deposition))

However, such a system cannot be used as a bottom DBR if we wish to realize a crystalline semiconductor microcavity (MC) unless wafer bonding techniques are employed to couple such a DBR to the cavity but it will involve lengthy processing steps to remove the DBR substrate.

(need for clean room facilities)

### b) AlAs / GaAs

The AlAs / GaAs couple is a nearly **strain-free** system as the two materials possess relatively similar lattice parameters so that crack-free DBRs with a high number of pairs and a peak reflectivity  $\sim 100\%$  can be obtained (while having a reduced dislocation density).

In addition, it is possible to oxidize the AlAs layers and therefore to have an oxide,  $\text{AlO}_x$ , which exhibits an optical refractive index much smaller than AlAs. As a result, AlAs / GaAs DBRs are characterized by a large stopband and can reach **high reflectivities** with a reduced number of pairs.

Such a couple is used to fabricate GaAs-based VCSELs emitting in the near IR. Due to the **bandgap** of GaAs, it is **not adapted for  $\lambda < 830\text{nm}$** .

### c) AlN / GaN

The AlN / GaN couple exhibits a **fairly large refractive index contrast** so that a priori a few number of pairs is required to get high reflectivity DBRs. However, contrary to its As - counterpart, the present couple is characterized by a **significant lattice parameter mismatch** which can lead to cracked structures and a high density of dislocations.

Usually the AlGaN/GaN system is preferred but it requires a much larger number of pairs due to the reduced optical refractive index contrast.

Alternatively, the AlInN/GaN system which is perfectly lattice matched for an indium content  $x_{In} \sim 18\%$  can also be used, but the AlInN alloy is difficult to grow.